



1st International Conference
Mathematical Modelling in Mechanics and Engineering
Mathematical Institute SANU, 8-10 September, 2022.



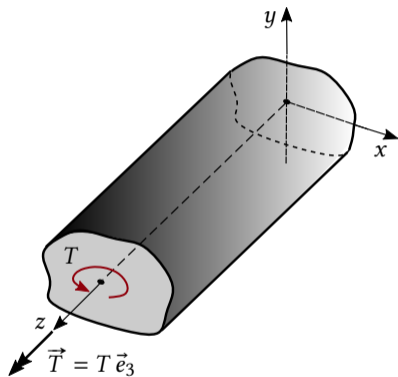
NUMERICAL COMPUTATIONS OF ELASTIC TORSION USING THE FINITE VOLUME METHOD

Aleksandar Čoćić (acocic@mas.bg.ac.rs)

University of Belgrade, Faculty of Mechanical Engineering, Chair for Fluid Mechanics

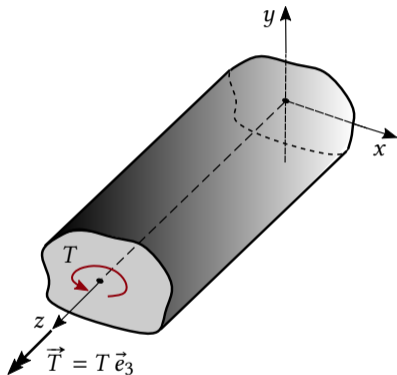
Physical Considerations: Formulation of the Problem

Cylindrical bar with arbitrary cross-section subjected to end loading moment.



Physical Considerations: Formulation of the Problem

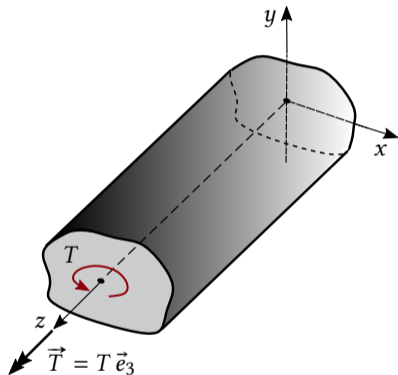
Cylindrical bar with arbitrary cross-section subjected to end loading moment.



Saint-Venant principle: seeking for the solution that satisfies the same resultant loading (not the pointwise traction conditions at the ends).

Physical Considerations: Formulation of the Problem

Cylindrical bar with arbitrary cross-section subjected to end loading moment.

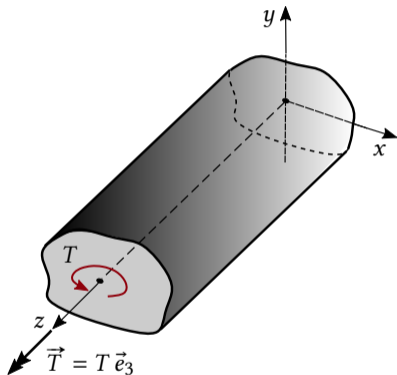


Reasonable assumptions:

Saint-Venant principle: seeking for the solution that satisfies the same resultant loading (not the pointwise traction conditions at the ends).

Physical Considerations: Formulation of the Problem

Cylindrical bar with arbitrary cross-section subjected to end loading moment.



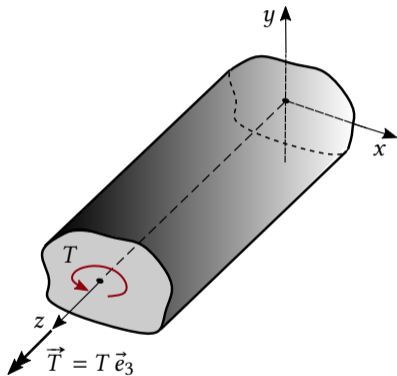
Reasonable assumptions:

- Each cross-section in (x, y) -plane rotates as rigid body around the central axis
- Amount of rotation is linear function of axial coordinate z (small deformation theory)

Saint-Venant principle: seeking for the solution that satisfies the same resultant loading (not the pointwise traction conditions at the ends).

Physical Considerations: Formulation of the Problem

Cylindrical bar with arbitrary cross-section subjected to end loading moment.

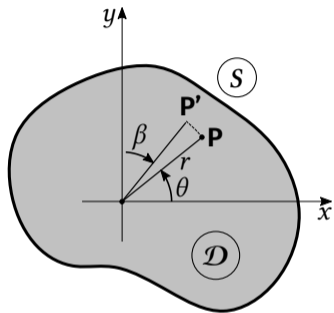


Reasonable assumptions:

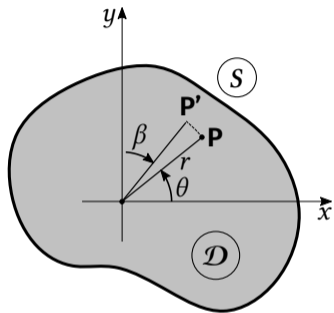
- Each cross-section in (x, y) -plane rotates as rigid body around the central axis
- Amount of rotation is linear function of axial coordinate z (small deformation theory)
- Circular cross-sections remain plane after deformation
- Plane cross-sections do not remain plane after deformation - warping displacement

Saint-Venant principle: seeking for the solution that satisfies the same resultant loading (not the pointwise traction conditions at the ends).

Mathematical Model: 2D Approach (Bar's Cross-section)

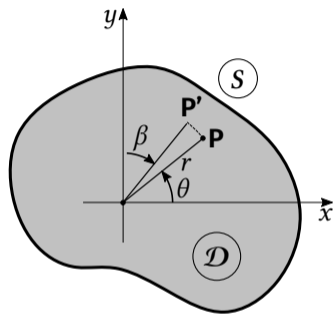


Mathematical Model: 2D Approach (Bar's Cross-section)



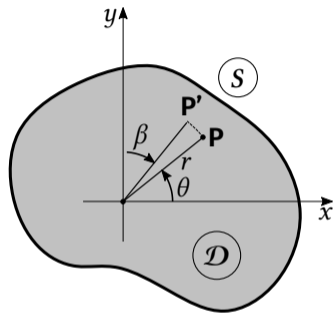
- Starting point: "known" displacement field
$$u = -\alpha zy, \quad v = \alpha xz, \quad w = \alpha w^*(x, y)$$
$$\alpha = \text{const} - \text{angle of twist per unit length}$$

Mathematical Model: 2D Approach (Bar's Cross-section)

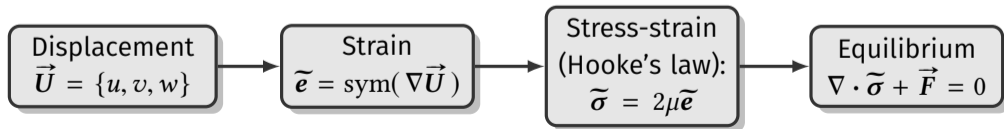


- Starting point: "known" displacement field
$$u = -\alpha zy, \quad v = \alpha xz, \quad w = \alpha w^*(x, y)$$
$$\alpha = \text{const} - \text{angle of twist per unit length}$$
- Displacement field must satisfy general equations of elasticity theory!

Mathematical Model: 2D Approach (Bar's Cross-section)



- Starting point: "known" displacement field
$$u = -\alpha zy, \quad v = \alpha xz, \quad w = \alpha w^*(x, y)$$
$$\alpha = \text{const} - \text{angle of twist per unit length}$$
- Displacement field must satisfy general equations of elasticity theory!



Various Formulations of Mathematical Model

Stress field:

$$\sigma_{ii} = 0, \tau_{yx} = \tau_{xy} = 0$$

$$\tau_{zx} = \tau_{xz} = \mu\alpha \left(\frac{\partial w^*}{\partial x} - y \right)$$

$$\tau_{zy} = \tau_{yz} = \mu\alpha \left(\frac{\partial w^*}{\partial y} + x \right)$$

Various Formulations of Mathematical Model

Stress field:

$$\sigma_{ii} = 0, \tau_{yx} = \tau_{xy} = 0$$

$$\tau_{zx} = \tau_{xz} = \mu\alpha \left(\frac{\partial w^*}{\partial x} - y \right)$$

$$\tau_{zy} = \tau_{yz} = \mu\alpha \left(\frac{\partial w^*}{\partial y} + x \right)$$

Equilibrium ($\vec{F} = 0$)

$$\nabla \cdot \tilde{\sigma} = 0$$

Various Formulations of Mathematical Model

Stress field:

$$\sigma_{ii} = 0, \tau_{yx} = \tau_{xy} = 0$$

$$\tau_{zx} = \tau_{xz} = \mu\alpha \left(\frac{\partial w^*}{\partial x} - y \right)$$

$$\tau_{zy} = \tau_{yz} = \mu\alpha \left(\frac{\partial w^*}{\partial y} + x \right)$$

Equilibrium ($\vec{F} = 0$)

$$\nabla \cdot \vec{\sigma} = 0$$

$$\frac{\partial \tau_{zx}}{\partial x} + \frac{\partial \tau_{zy}}{\partial y} = 0$$

Various Formulations of Mathematical Model

Stress field:

$$\sigma_{ii} = 0, \tau_{yx} = \tau_{xy} = 0$$

$$\tau_{zx} = \tau_{xz} = \mu\alpha \left(\frac{\partial w^*}{\partial x} - y \right)$$

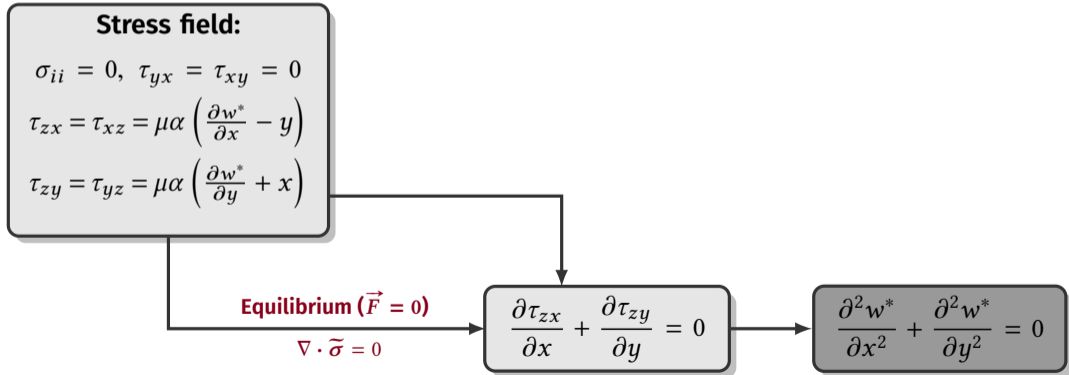
$$\tau_{zy} = \tau_{yz} = \mu\alpha \left(\frac{\partial w^*}{\partial y} + x \right)$$

Equilibrium ($\vec{F} = 0$)

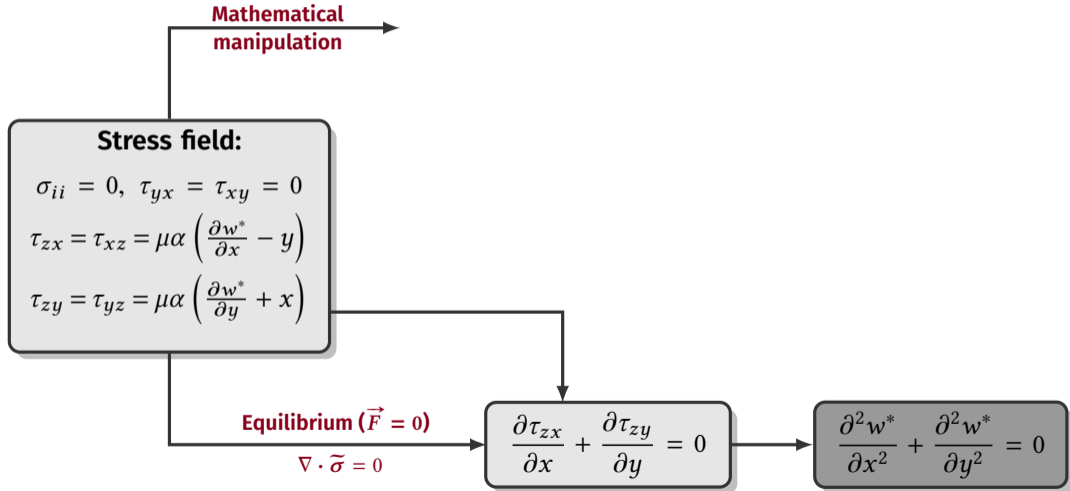
$$\nabla \cdot \vec{\sigma} = 0$$

$$\frac{\partial \tau_{zx}}{\partial x} + \frac{\partial \tau_{zy}}{\partial y} = 0$$

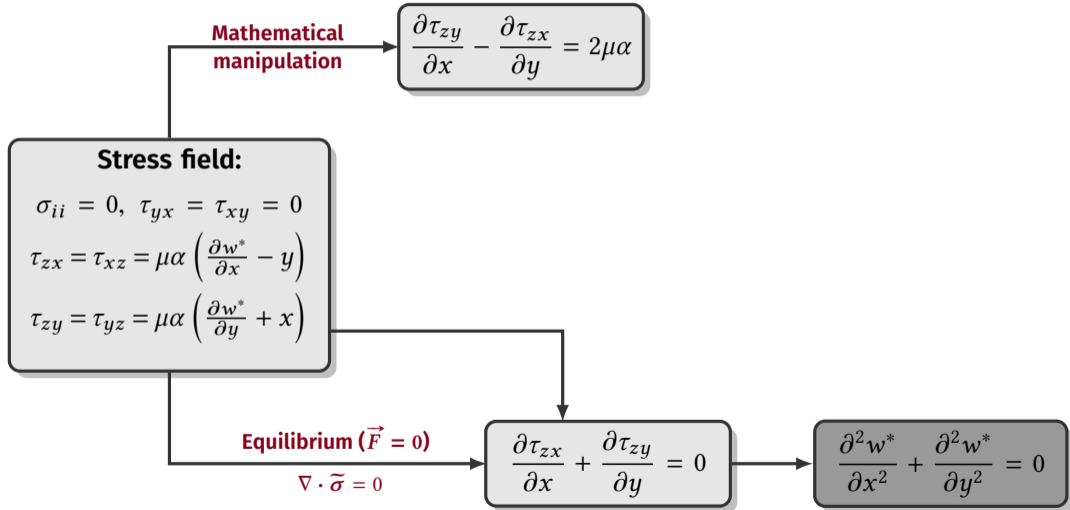
Various Formulations of Mathematical Model



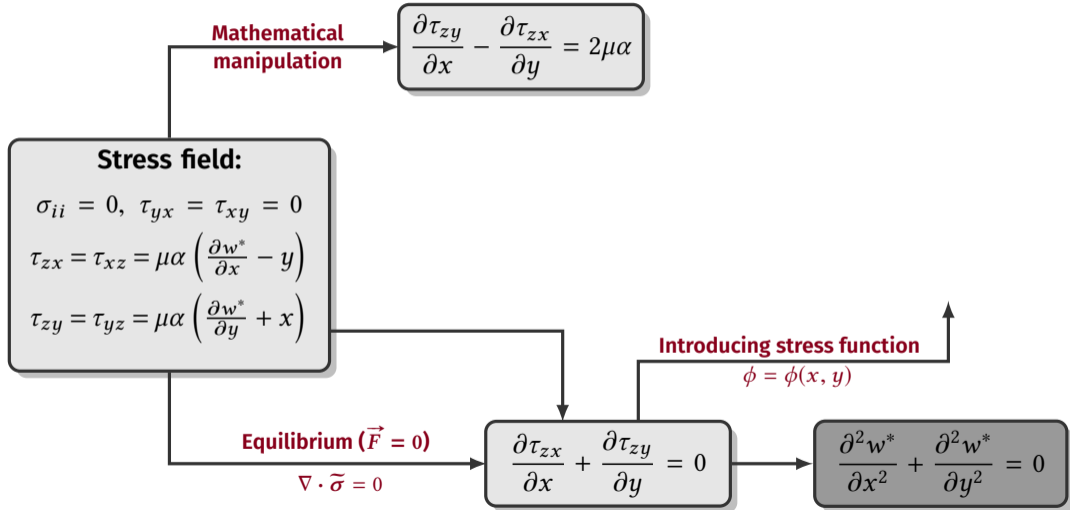
Various Formulations of Mathematical Model



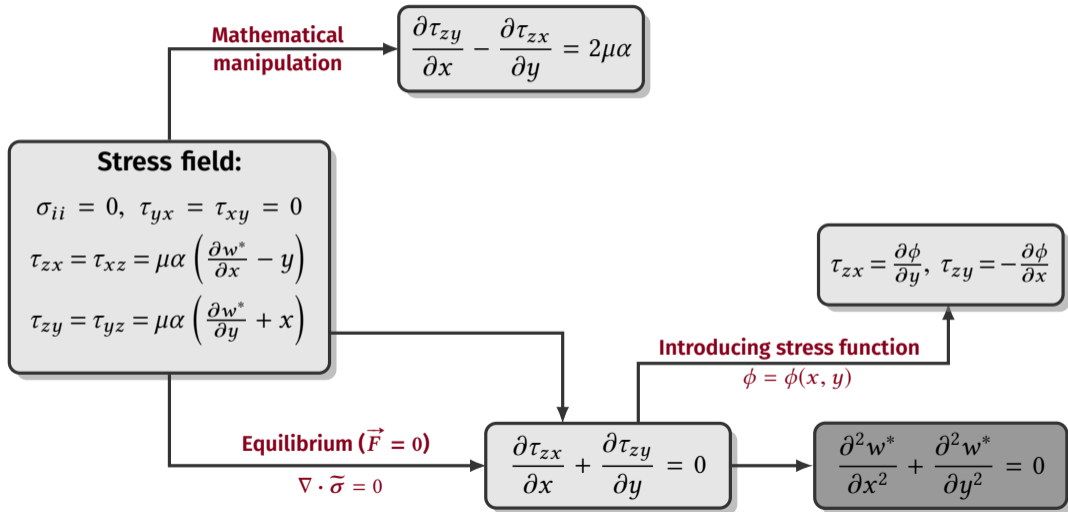
Various Formulations of Mathematical Model



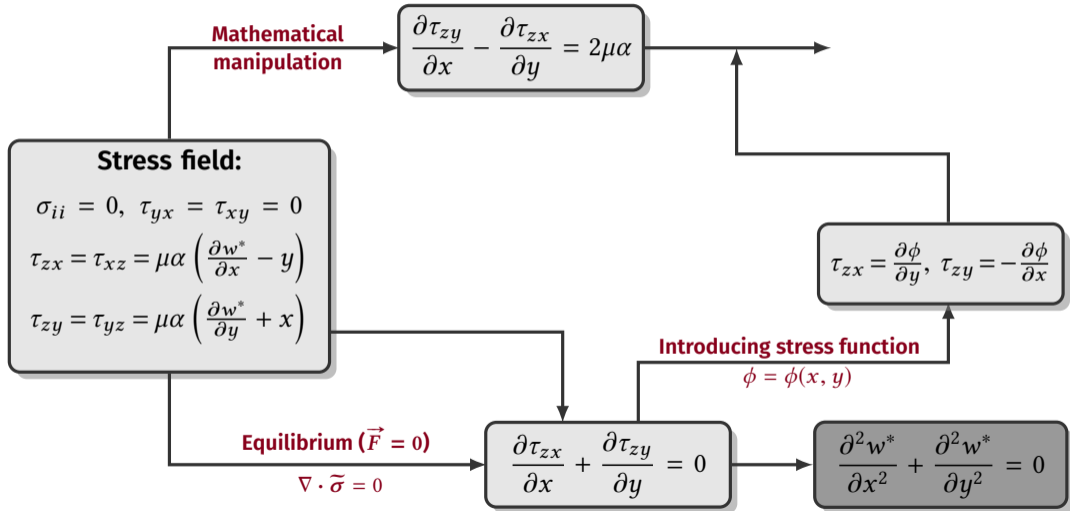
Various Formulations of Mathematical Model



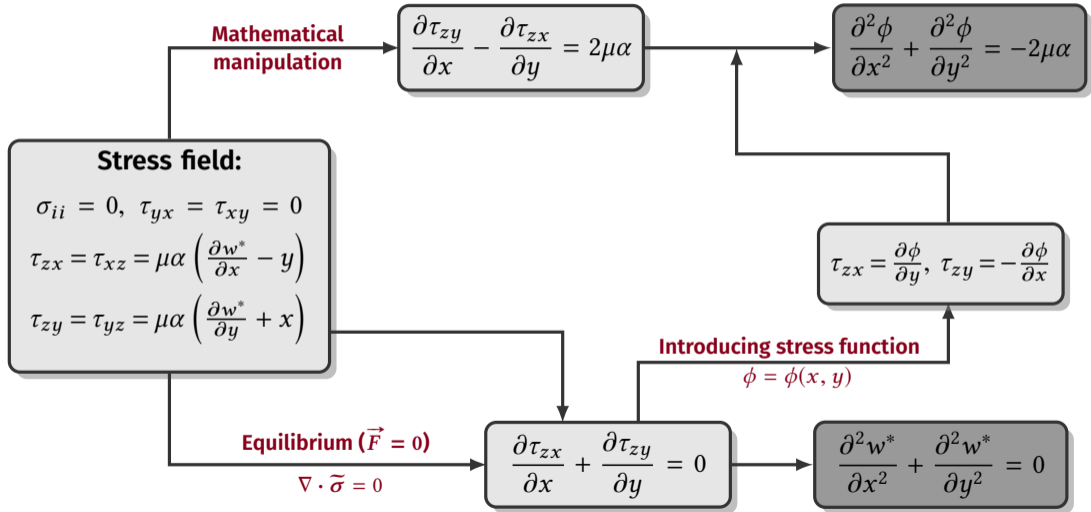
Various Formulations of Mathematical Model



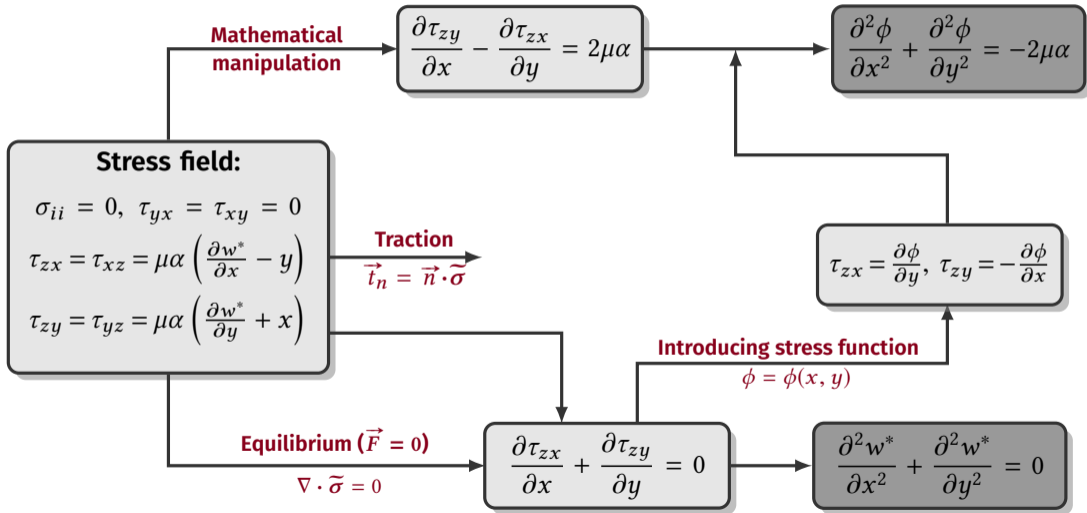
Various Formulations of Mathematical Model



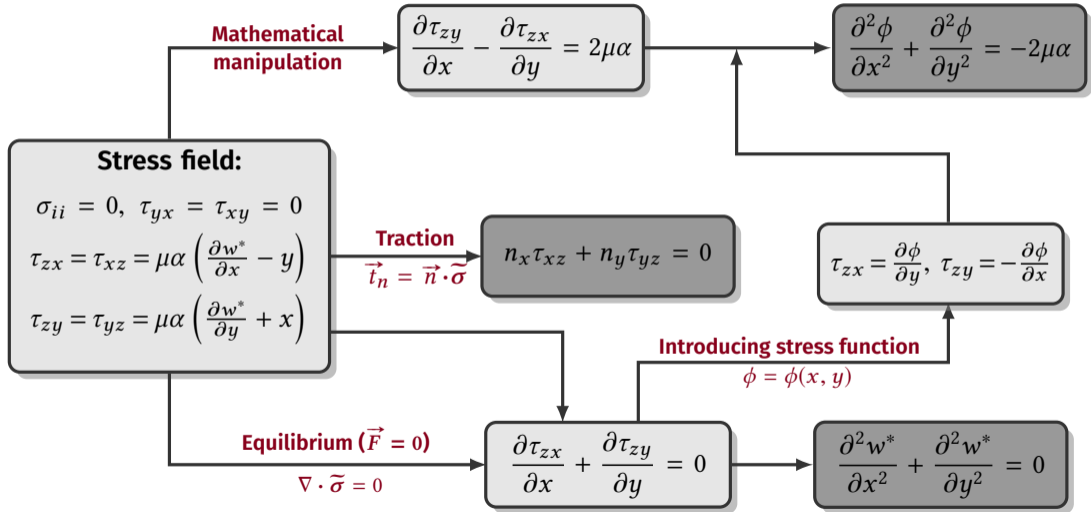
Various Formulations of Mathematical Model



Various Formulations of Mathematical Model



Various Formulations of Mathematical Model



Final Formulation, With Simple Scaling: $\tau_{zx}/(\mu\alpha) = \tau_x$, $\tau_{zy}/(\mu\alpha) = \tau_y$

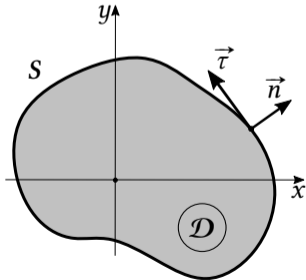
Elliptic type

Laplace's PDE:

$$\nabla^2 w^* = 0$$

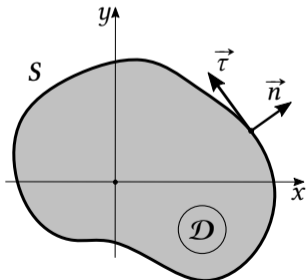
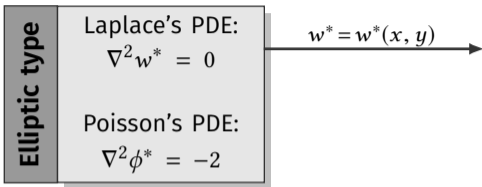
Poisson's PDE:

$$\nabla^2 \phi^* = -2$$



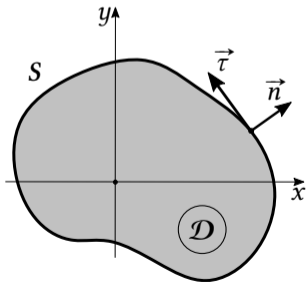
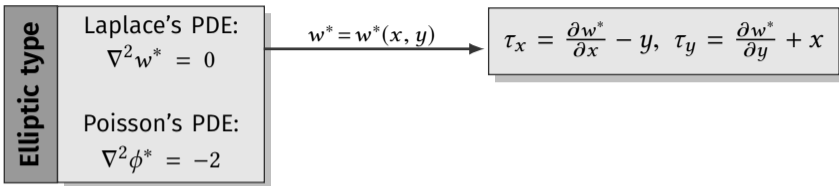
Simple-connected domain

Final Formulation, With Simple Scaling: $\tau_{zx}/(\mu\alpha) = \tau_x$, $\tau_{zy}/(\mu\alpha) = \tau_y$



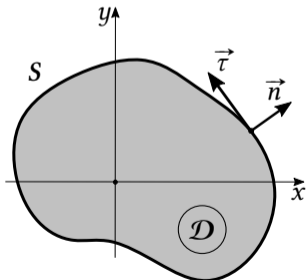
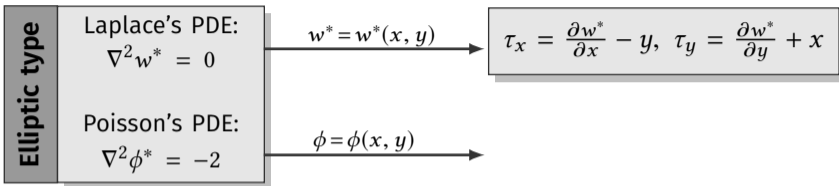
Simple-connected domain

Final Formulation, With Simple Scaling: $\tau_{zx}/(\mu\alpha) = \tau_x$, $\tau_{zy}/(\mu\alpha) = \tau_y$



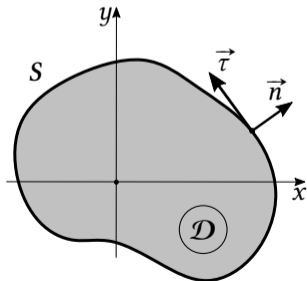
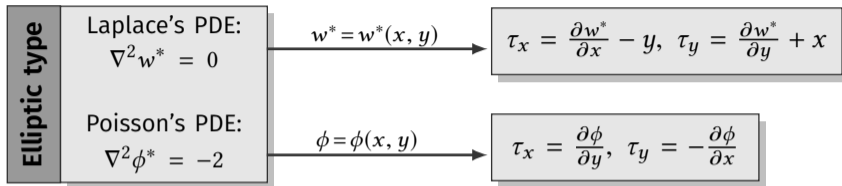
Simple-connected domain

Final Formulation, With Simple Scaling: $\tau_{zx}/(\mu\alpha) = \tau_x$, $\tau_{zy}/(\mu\alpha) = \tau_y$



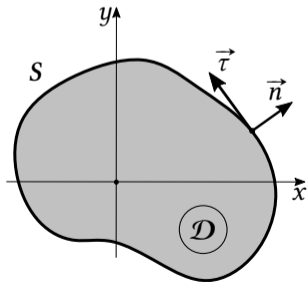
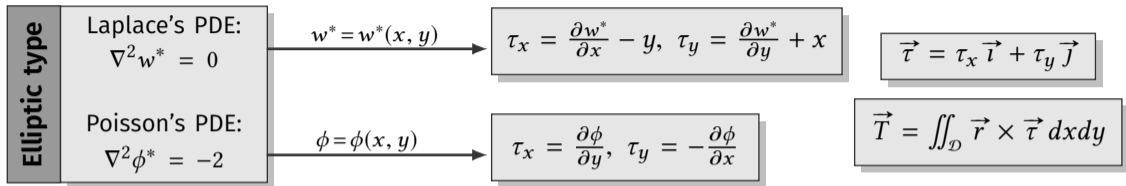
Simple-connected domain

Final Formulation, With Simple Scaling: $\tau_{zx}/(\mu\alpha) = \tau_x$, $\tau_{zy}/(\mu\alpha) = \tau_y$



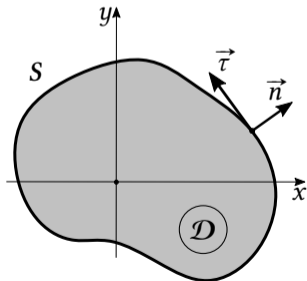
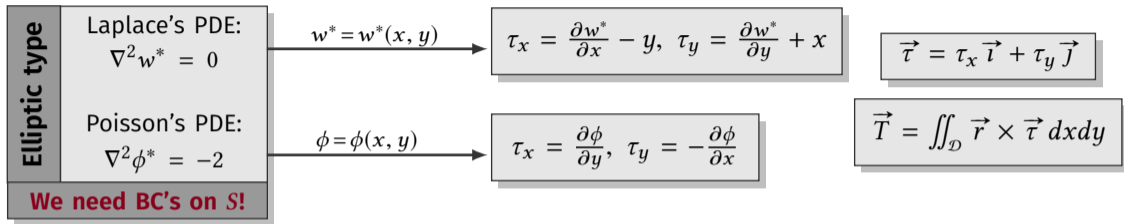
Simple-connected domain

Final Formulation, With Simple Scaling: $\tau_{zx}/(\mu\alpha) = \tau_x$, $\tau_{zy}/(\mu\alpha) = \tau_y$



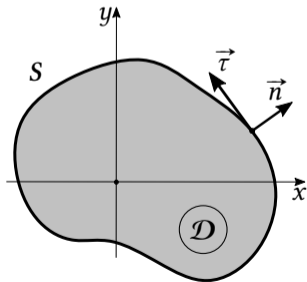
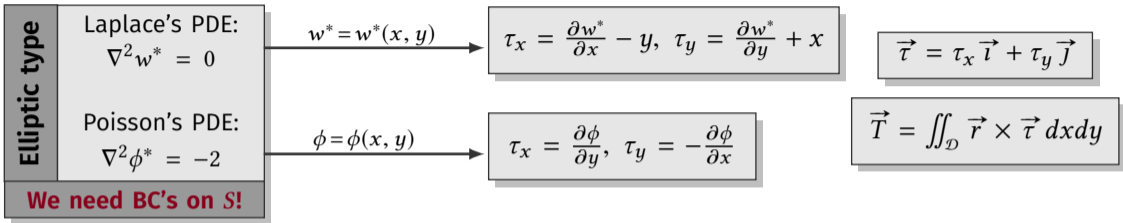
Simple-connected domain

Final Formulation, With Simple Scaling: $\tau_{zx}/(\mu\alpha) = \tau_x$, $\tau_{zy}/(\mu\alpha) = \tau_y$



Simple-connected domain

Final Formulation, With Simple Scaling: $\tau_{zx}/(\mu\alpha) = \tau_x, \tau_{zy}/(\mu\alpha) = \tau_y$

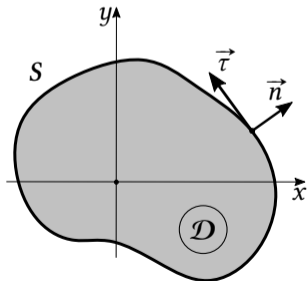
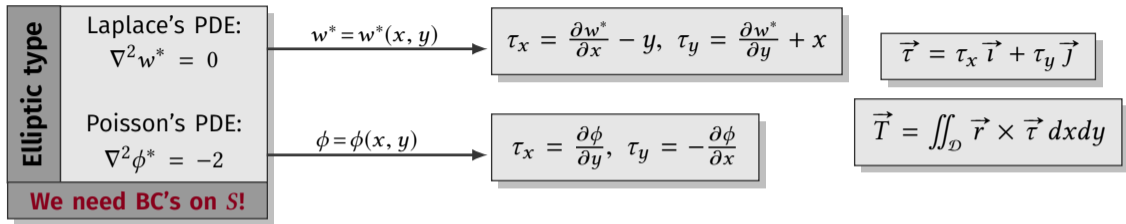


Simple-connected domain

Physical condition on S: zero traction

On S:
 $\vec{\tau} \cdot \vec{n} = 0$

Final Formulation, With Simple Scaling: $\tau_{zx}/(\mu\alpha) = \tau_x$, $\tau_{zy}/(\mu\alpha) = \tau_y$

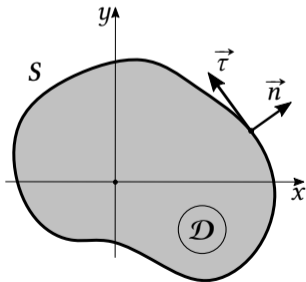
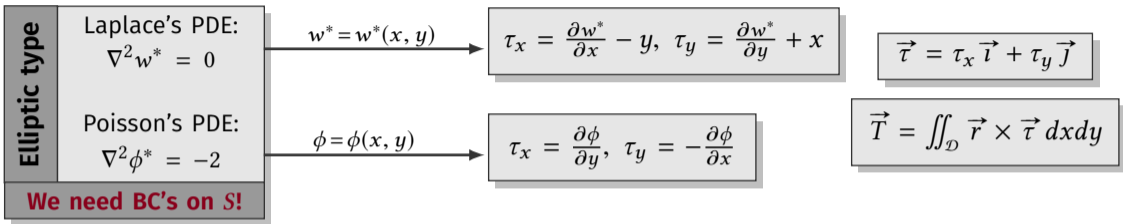


Simple-connected domain

Physical condition on S: zero traction

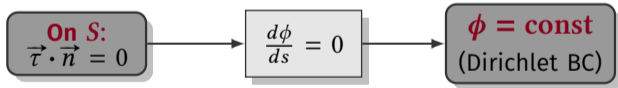
On S: $\vec{\tau} \cdot \vec{n} = 0$	$\frac{d\phi}{ds} = 0$
--	------------------------

Final Formulation, With Simple Scaling: $\tau_{zx}/(\mu\alpha) = \tau_x$, $\tau_{zy}/(\mu\alpha) = \tau_y$

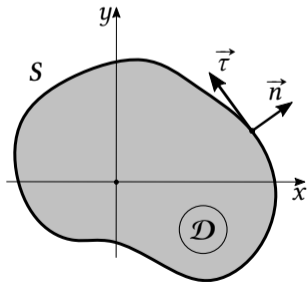
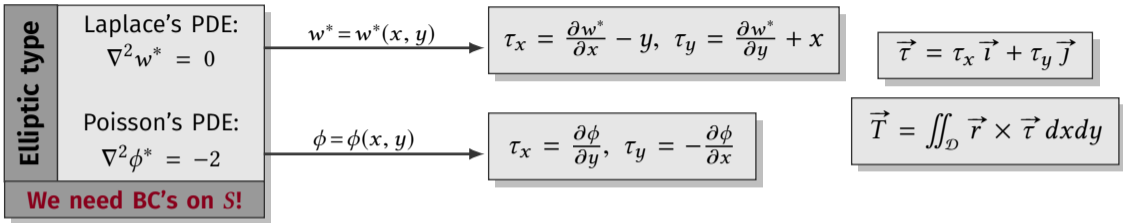


Simple-connected domain

Physical condition on S : zero traction

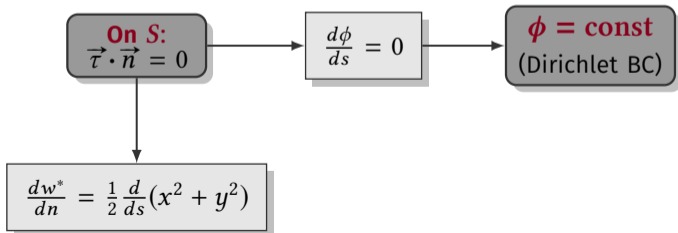


Final Formulation, With Simple Scaling: $\tau_{zx}/(\mu\alpha) = \tau_x$, $\tau_{zy}/(\mu\alpha) = \tau_y$

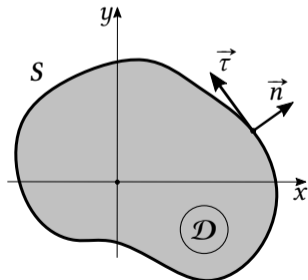
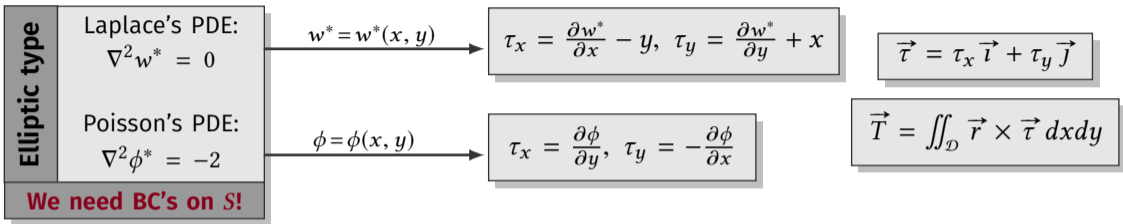


Simple-connected domain

Physical condition on S : zero traction

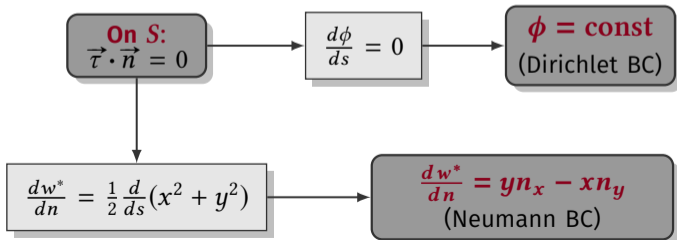


Final Formulation, With Simple Scaling: $\tau_{zx}/(\mu\alpha) = \tau_x$, $\tau_{zy}/(\mu\alpha) = \tau_y$



Simple-connected domain

Physical condition on S: zero traction



Final Formulation, With Simple Scaling: $\tau_{zx}/(\mu\alpha) = \tau_x$, $\tau_{zy}/(\mu\alpha) = \tau_y$

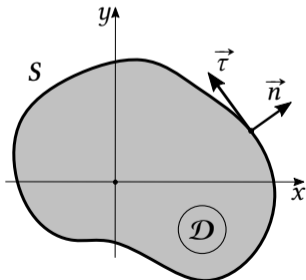
Elliptic type

Laplace's PDE:

$$\nabla^2 w^* = 0$$

Poisson's PDE:

$$\nabla^2 \phi^* = -2$$



Simple-connected domain

Physical condition on S : zero traction

$$\text{On } S: \vec{\tau} \cdot \vec{n} = 0$$

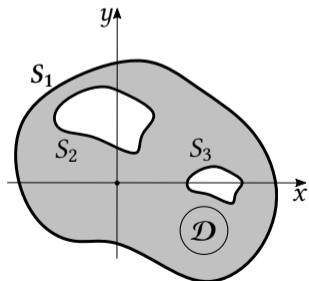
$$\phi = \text{const} \\ \text{(Dirichlet BC)}$$

$$\frac{dw^*}{dn} = yn_x - xn_y \\ \text{(Neumann BC)}$$

Additional Generalization: What if We Have Hollow Cylinder

Additional Generalization: What if We Have Hollow Cylinder

Elliptic type	Laplace's PDE: $\nabla^2 w^* = 0$
	Poisson's PDE: $\nabla^2 \phi^* = -2$

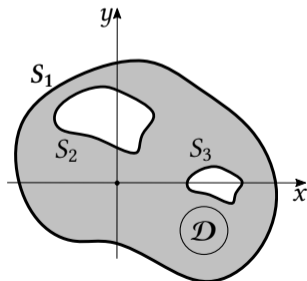


Multiply-connected domain

Additional Generalization: What if We Have Hollow Cylinder

Elliptic type	Laplace's PDE: $\nabla^2 w^* = 0$
	Poisson's PDE: $\nabla^2 \phi^* = -2$

The same physical condition: no traction on each contour
→ boundary conditions on S_i :



Multiply-connected domain

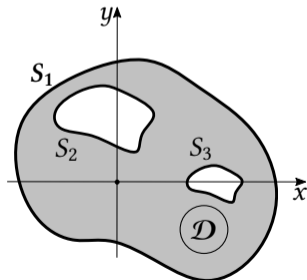
Additional Generalization: What if We Have Hollow Cylinder

Elliptic type	Laplace's PDE: $\nabla^2 w^* = 0$
	Poisson's PDE: $\nabla^2 \phi^* = -2$

The same physical condition: no traction on each contour
→ boundary conditions on S_i :

$$\phi = C_i \rightarrow \text{different values of constant } C_i!$$

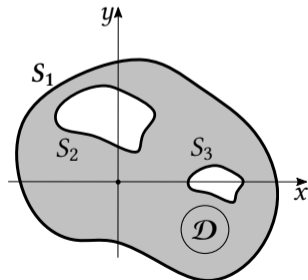
$$\frac{dw^*}{dn} = yn_x - xn_y \rightarrow \text{geometry of the contour } S_i$$



Multiply-connected domain

Additional Generalization: What if We Have Hollow Cylinder

Elliptic type	Laplace's PDE: $\nabla^2 w^* = 0$
	Poisson's PDE: $\nabla^2 \phi^* = -2$



Multiply-connected domain

The same physical condition: no traction on each contour
→ boundary conditions on S_i :

$$\phi = C_i \rightarrow \text{different values of constant } C_i!$$

$$\frac{dw^*}{dn} = yn_x - xn_y \rightarrow \text{geometry of the contour } S_i$$

Problem: values of C_i are not known in advance!

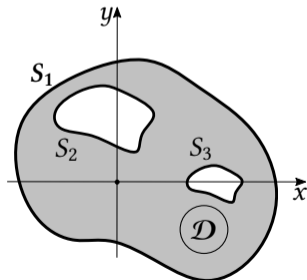
Additional Generalization: What if We Have Hollow Cylinder

Elliptic type	Laplace's PDE: $\nabla^2 w^* = 0$
	Poisson's PDE: $\nabla^2 \phi^* = -2$

The same physical condition: no traction on each contour
→ boundary conditions on S_i :

$$\phi = C_i \rightarrow \text{different values of constant } C_i!$$

$$\frac{dw^*}{dn} = yn_x - xn_y \rightarrow \text{geometry of the contour } S_i$$



Multiply-connected domain

Problem: values of C_i are not known in advance!

- Green's theorem can't help much:

$$\oint_{S_i} \vec{\tau} \cdot d\vec{s} = \iint_{A_i} \underbrace{\nabla \times \vec{\tau}}_{=2} dA \rightarrow \oint_{S_i} \vec{\tau} \cdot d\vec{s} = 2A_i$$

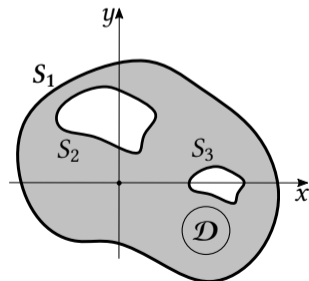
Additional Generalization: What if We Have Hollow Cylinder

Elliptic type	Laplace's PDE: $\nabla^2 w^* = 0$
	Poisson's PDE: $\nabla^2 \phi^* = -2$

The same physical condition: no traction on each contour
 \rightarrow boundary conditions on S_i :

$$\phi = C_i \quad \rightarrow \quad \text{different values of constant } C_i!$$

$$\frac{dw^*}{dn} = yn_x - xn_y \quad \rightarrow \quad \text{geometry of the contour } S_i$$



Multiply-connected domain

Problem: values of C_i are not known in advance!

- Green's theorem can't help much:

$$\oint_{S_i} \vec{\tau} \cdot d\vec{s} = \iint_{A_i} \underbrace{\nabla \times \vec{\tau}}_{=2} dA \quad \rightarrow \quad \oint_{S_i} \vec{\tau} \cdot d\vec{s} = 2A_i$$

$$\vec{\tau} \parallel d\vec{s} \quad (\vec{\tau} = \tau \vec{e}_s) \quad \rightarrow \quad \oint_{S_i} \tau ds = \oint_{S_i} \frac{d\phi}{dn} ds = 2A_i$$

Finite Volume Method (FVM): Numerical Method for Solving of PDE's

- Natural method of discretization for PDE's written in strong conservative form (fluid mechanics usually, but it can be also used for solid mechanics!)

Finite Volume Method (FVM): Numerical Method for Solving of PDE's

- Natural method of discretization for PDE's written in strong conservative form (fluid mechanics usually, but it can be also used for solid mechanics!)
- General transport equation for quantity φ in fluid flow field

$$\frac{\partial(\rho\varphi)}{\partial t} + \nabla \cdot (\rho\vec{U}\varphi) = \nabla \cdot (\Gamma\nabla\varphi) + S_\varphi$$

Finite Volume Method (FVM): Numerical Method for Solving of PDE's

- Natural method of discretization for PDE's written in strong conservative form (fluid mechanics usually, but it can be also used for solid mechanics!)
- General transport equation for quantity φ in fluid flow field

$$\frac{\partial(\rho\varphi)}{\partial t} + \nabla \cdot (\rho\vec{U}\varphi) = \nabla \cdot (\Gamma\nabla\varphi) + S_\varphi$$

- Integration over volume V and application of Ostrogradsky-Gauss theorem

$$\iiint_V \frac{\partial(\rho\varphi)}{\partial t} dV + \iint_A \vec{n} \cdot (\rho\varphi\vec{U}) dA = \iint_A \vec{n} \cdot (\Gamma\nabla\varphi) dA + \iiint_V S_T dV$$

Finite Volume Method (FVM): Numerical Method for Solving of PDE's

- Natural method of discretization for PDE's written in strong conservative form (fluid mechanics usually, but it can be also used for solid mechanics!)
- General transport equation for quantity φ in fluid flow field

$$\frac{\partial(\rho\varphi)}{\partial t} + \nabla \cdot (\rho\vec{U}\varphi) = \nabla \cdot (\Gamma\nabla\varphi) + S_\varphi$$

- Integration over volume V and application of Ostrogradsky-Gauss theorem

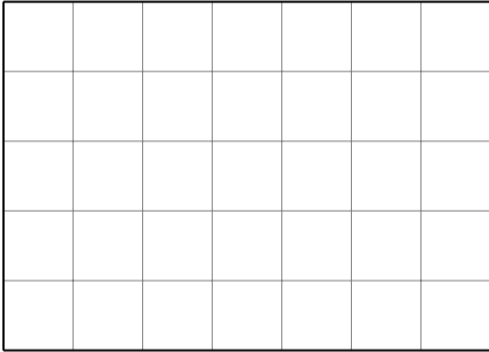
$$\iiint_V \frac{\partial(\rho\varphi)}{\partial t} dV + \iint_A \vec{n} \cdot (\rho\varphi\vec{U}) dA = \iint_A \vec{n} \cdot (\Gamma\nabla\varphi) dA + \iiint_V S_T dV$$

- Pure steady-state diffusion, without source term

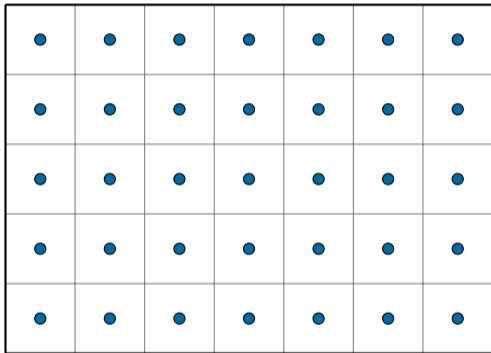
$$\iint_A \vec{n} \cdot (\Gamma\nabla\varphi) dA = 0 \quad \rightarrow \quad \text{for } \Gamma = \text{const} \quad \rightarrow \quad \iint_A \vec{n} \cdot \nabla\varphi dA = 0 \quad (\text{PDE: } \nabla^2\varphi = 0)$$

FVM: General Principle of Discretization of Computational Domain

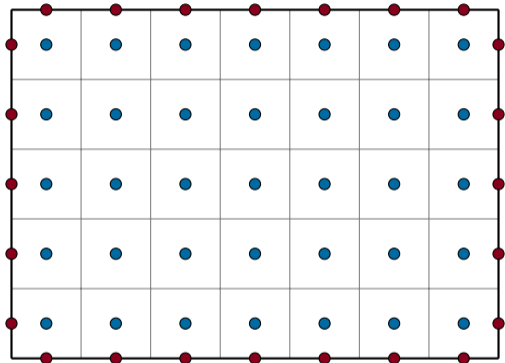
FVM: General Principle of Discretization of Computational Domain



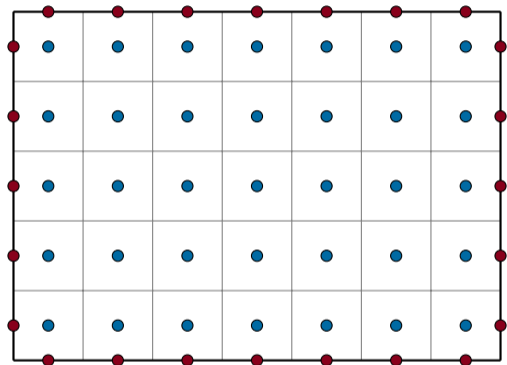
FVM: General Principle of Discretization of Computational Domain



FVM: General Principle of Discretization of Computational Domain

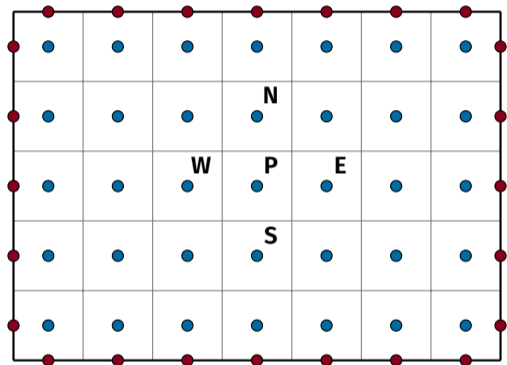


FVM: General Principle of Discretization of Computational Domain



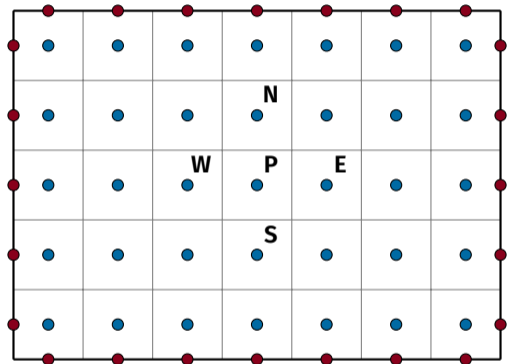
- Boundary conditions
- Computational points

FVM: General Principle of Discretization of Computational Domain



- Boundary conditions
- Computational points

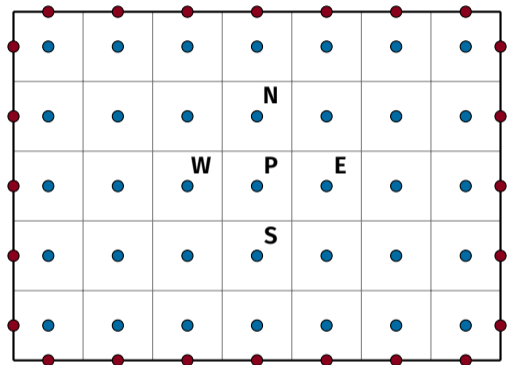
FVM: General Principle of Discretization of Computational Domain



- Boundary conditions
- Computational points

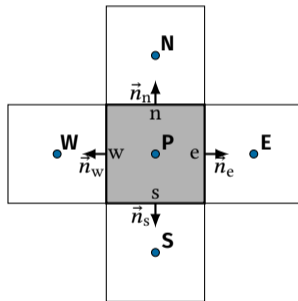
P - centroid of computational cell (point)
W, E, N, S - centroids of neighbouring cells

FVM: General Principle of Discretization of Computational Domain

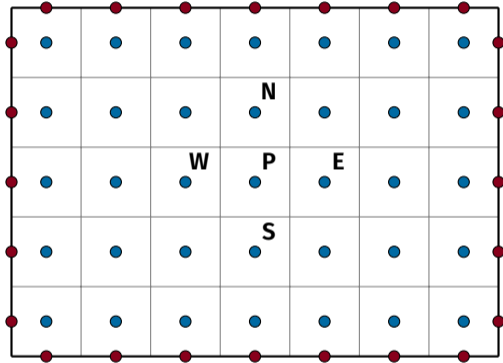


- Boundary conditions
- Computational points

P - centroid of computational cell (point)
W, E, N, S - centroids of neighbouring cells

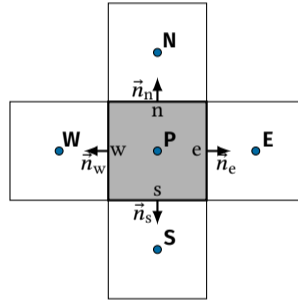


FVM: General Principle of Discretization of Computational Domain



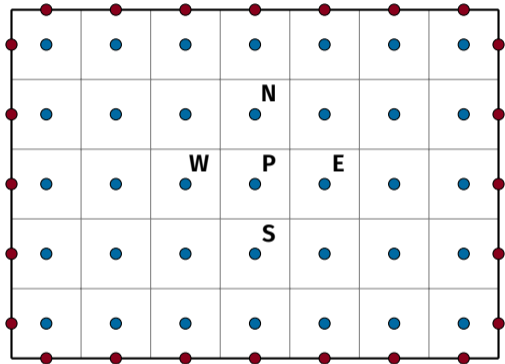
- Boundary conditions
- Computational points

P - centroid of computational cell (point)
W, E, N, S - centroids of neighbouring cells



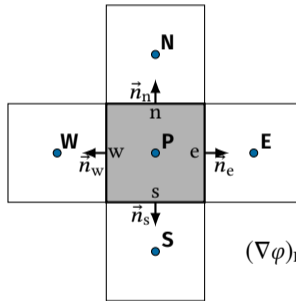
$$\oiint_A \vec{n} \cdot \nabla \varphi \, dA = \sum_k \iint_{A_k} \vec{n} \cdot \nabla \varphi \, dA, \quad k = e, w, n, s$$

FVM: General Principle of Discretization of Computational Domain



- Boundary conditions
- Computational points

P - centroid of computational cell (point)
W, E, N, S - centroids of neighbouring cells



$$(\nabla\varphi)_P = \frac{1}{V_P} \sum_f \vec{n}_f \varphi_f A_f$$

$$\oiint_A \vec{n} \cdot \nabla\varphi \, dA = \sum_k \iint_{A_k} \vec{n} \cdot \nabla\varphi \, dA, \quad k = e, w, n, s$$

Analysis of the Problem and Numerical Methods: Done! Implementation Follows

Analysis of the Problem and Numerical Methods: Done! Implementation Follows

- **Open-source philosophy:** use existing codes and suite them for your needs

```
const volVectorField& C = mesh.C();
const surfaceVectorField& Sf = mesh.Sf();
volVectorField coord = -C.component(vector::Y)*ei + C.
    component(vector::X)*ej;

fvScalarMatrix WEqn
(
    fvm::ddt(W) - fvm::laplacian(k, W)
);
WEqn.relax();
WEqn.solve();

tau = fvc::grad(W) + coord;
phi = fvc::interpolate(tau) & Sf;
magTau =mag(tau);
```

```
const fvPatch& boundaryPatch = patch();
const vectorField& Cf = boundaryPatch.Cf();
// Vektori normala na granicnoj povrsi
const vectorField& Sf = boundaryPatch.Sf();
// Povrsine pojedinačnih povrsi
const scalarField& magSf = boundaryPatch.magSf();
scalarField& field = this->refGrad();
forAll(Cf, faceI)
{
    const scalar x = Cf[faceI].x();
    const scalar y = Cf[faceI].y();
    const scalar nx = Sf[faceI].x()/magSf[faceI];
    const scalar ny = Sf[faceI].y()/magSf[faceI];
    field[faceI] = y*nx - x*ny;
}
```

Analysis of the Problem and Numerical Methods: Done! Implementation Follows

- **Open-source philosophy:** use existing codes and suite them for your needs
- **OpenFOAM:** huge collection of C++ libraries for CCM (based on FVM)

```
const volVectorField& C = mesh.C();
const surfaceVectorField& Sf = mesh.Sf();
volVectorField coord = -C.component(vector::Y)*ei + C.
    component(vector::X)*ej;

fvScalarMatrix WEqn
(
    fvm::ddt(W) - fvm::laplacian(k, W)
);
WEqn.relax();
WEqn.solve();

tau = fvc::grad(W) + coord;
phi = fvc::interpolate(tau) & Sf;
magTau =mag(tau);
```

```
const fvPatch& boundaryPatch = patch();
const vectorField& Cf = boundaryPatch.Cf();
// Vektori normala na granicnoj povrsi
const vectorField& Sf = boundaryPatch.Sf();
// Povrsine pojedinačnih povrsi
const scalarField& magSf = boundaryPatch.magSf();
scalarField& field = this->refGrad();
forAll(Cf, faceI)
{
    const scalar x = Cf[faceI].x();
    const scalar y = Cf[faceI].y();
    const scalar nx = Sf[faceI].x()/magSf[faceI];
    const scalar ny = Sf[faceI].y()/magSf[faceI];
    field[faceI] = y*nx - x*ny;
}
```

Analysis of the Problem and Numerical Methods: Done! Implementation Follows

- **Open-source philosophy:** use existing codes and suite them for your needs
- **OpenFOAM:** huge collection of C++ libraries for CCM (based on FVM)
- Modification of the solver `laplacianFoam`, create `torsionWarpingFoam`, with additional implementation for boundary condition

```
const volVectorField& C = mesh.C();
const surfaceVectorField& Sf = mesh.Sf();
volVectorField coord = -C.component(vector::Y)*ei + C.
    component(vector::X)*ej;

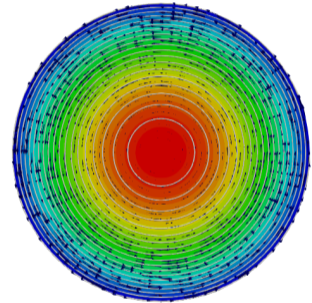
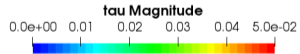
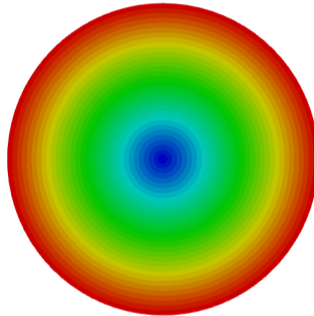
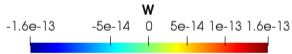
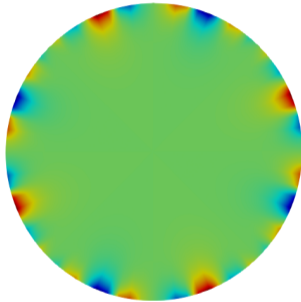
fvScalarMatrix WEqn
(
    fvm::ddt(W) - fvm::laplacian(k, W)
);
WEqn.relax();
WEqn.solve();

tau = fvc::grad(W) + coord;
phi = fvc::interpolate(tau) & Sf;
magTau =mag(tau);
```

```
const fvPatch& boundaryPatch = patch();
const vectorField& Cf = boundaryPatch.Cf();
// Vektori normala na granicnoj povrsi
const vectorField& Sf = boundaryPatch.Sf();
// Povrsine pojedinačnih povrsi
const scalarField& magSf = boundaryPatch.magSf();
scalarField& field = this->refGrad();
forAll(Cf, faceI)
{
    const scalar x = Cf[faceI].x();
    const scalar y = Cf[faceI].y();
    const scalar nx = Sf[faceI].x()/magSf[faceI];
    const scalar ny = Sf[faceI].y()/magSf[faceI];
    field[faceI] = y*nx - x*ny;
}
```

Simple Cases, Known Analytical Solution - Circle And Square Domain

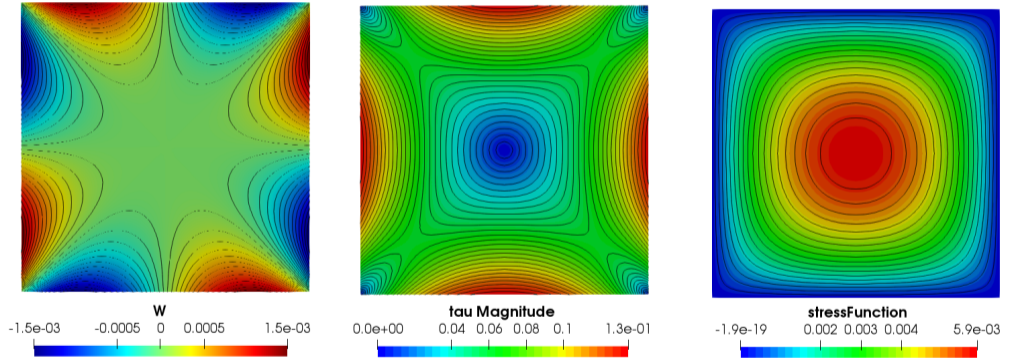
- **Circle:** distribution of warping function, stress vectors, and stress function



- Perfect agreement with analytical solution

Simple Cases, Known Analytical Solution - Circle And Square Domain

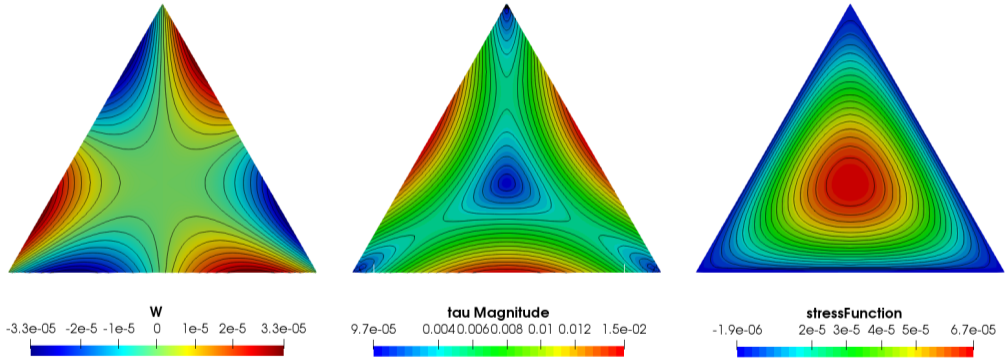
- **Square:** distribution of warping function, stress vectors, and stress function



- Perfect agreement with analytical solution

Simple Cases, Known Analytical Solution - Equilateral Triangle

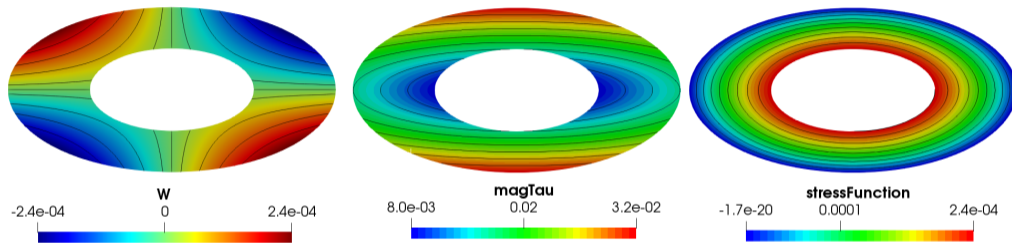
- **Equilateral triangle:** distribution of warping function, stress vectors, and stress function



- Perfect agreement with analytical solution

Multiply-connected Domains: Hollow Ellipse (Known Analytical Solution)

- Geometrical characteristics: $a/b = 2, k = 0.5$ (outer ellipse $a = 4$ cm, $b = 2$ cm)

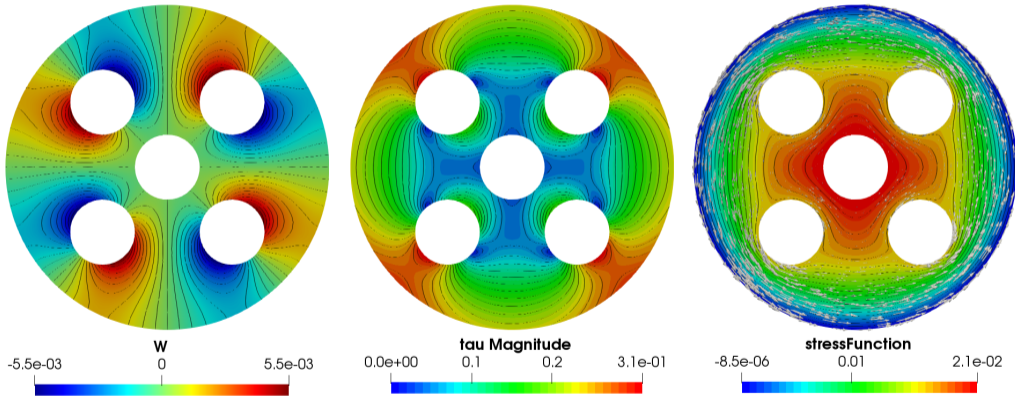


- Analytical solution for torque (torsional constant): $\frac{T}{\mu\alpha} = \frac{a^3 b^3 \pi}{a^2 + b^2} (1 - k^4) = 75.39822 \text{ cm}^4$
- Numerical solution: based on solved distribution for w^* and numerical integration:

$$\frac{T}{\mu\alpha} = \underbrace{\iint_{\mathcal{D}} \left(x^2 + y^2 + x \frac{\partial w^*}{\partial y} - y \frac{\partial w^*}{\partial x} \right) dx dy}_{F} \rightarrow [\text{fvc::domainIntegrate}(F)] \rightarrow 75.38238 \text{ cm}^4$$

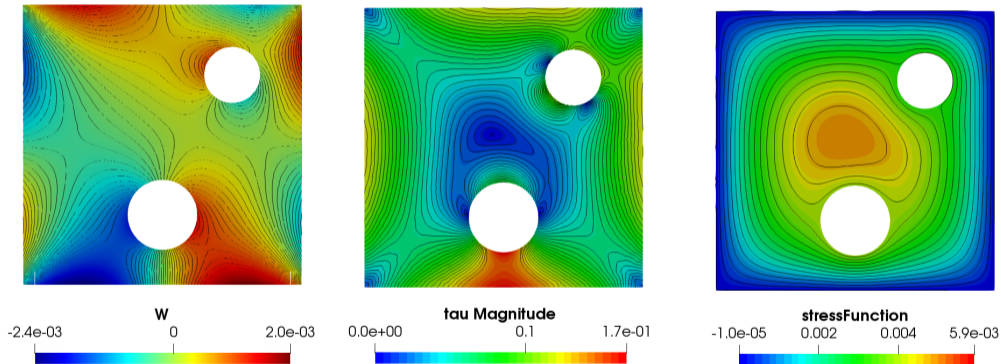
Multiply-connected Domains: Playing Around With Some Random Shapes

- Domain symmetry - symmetry in solution (well known and expected)

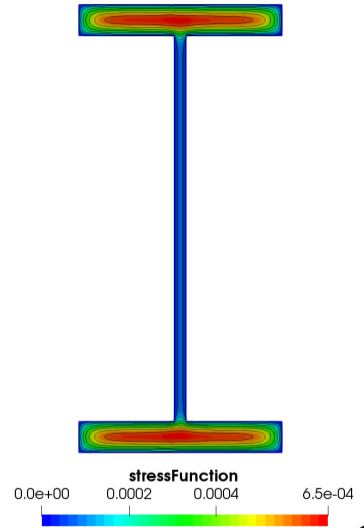
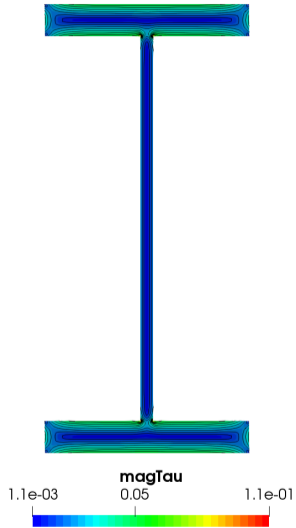
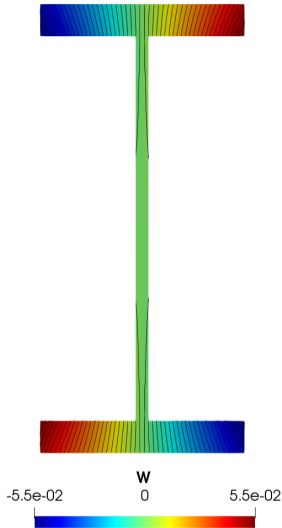


Multiply-connected Domains: Playing Around With Some Random Shapes

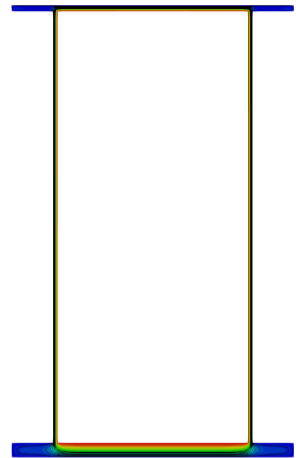
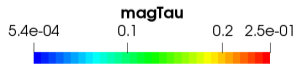
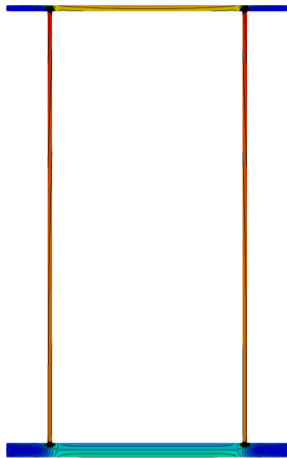
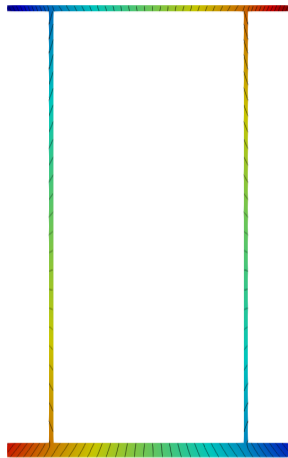
- Domain asymmetry - asymmetry in solution (well known and expected)



Practical, Engineering Applications (Thin-walled Cross-sections)



Practical, Engineering Applications (Thin-walled Cross-sections)



Summary

- Problem of elastic torsion is analyzed using Saint-Venant principle

Summary

- Problem of elastic torsion is analyzed using Saint-Venant principle
- Obtained Laplace's PDE with inhomogeneous Neumann BC is solved numerically using finite volume method

Summary

- Problem of elastic torsion is analyzed using Saint-Venant principle
- Obtained Laplace's PDE with inhomogeneous Neumann BC is solved numerically using finite volume method

Summary

- Problem of elastic torsion is analyzed using Saint-Venant principle
- Obtained Laplace's PDE with inhomogeneous Neumann BC is solved numerically using finite volume method
- OpenFOAM tools are used for that purpose, and new solver is created

Summary

- Problem of elastic torsion is analyzed using Saint-Venant principle
- Obtained Laplace's PDE with inhomogeneous Neumann BC is solved numerically using finite volume method
- OpenFOAM tools are used for that purpose, and new solver is created
- This is very simple and rather isolated approach for numerical studies of solid mechanics (torsion problem), but (for those interested)

Summary

- Problem of elastic torsion is analyzed using Saint-Venant principle
- Obtained Laplace's PDE with inhomogeneous Neumann BC is solved numerically using finite volume method
- OpenFOAM tools are used for that purpose, and new solver is created
- This is very simple and rather isolated approach for numerical studies of solid mechanics (torsion problem), but (for those interested)
- Check out the work of Aleksandar Karač, Željko Tuković, Hrvoje Jasak, Philip Cardiff, Declan Carolan, Michael Leonard and Valentine Kanyanta:

Summary

- Problem of elastic torsion is analyzed using Saint-Venant principle
- Obtained Laplace's PDE with inhomogeneous Neumann BC is solved numerically using finite volume method
- OpenFOAM tools are used for that purpose, and new solver is created
- This is very simple and rather isolated approach for numerical studies of solid mechanics (torsion problem), but (for those interested)
- Check out the work of Aleksandar Karač, Željko Tuković, Hrvoje Jasak, Philip Cardiff, Declan Carolan, Michael Leonard and Valentine Kanyanta:

SOLID MECHANICS - FINITE VOLUME SOLVERS

<https://github.com/wyldckat/solidMechanics>